



VB027ASP

HIGH VOLTAGE IGNITION COIL DRIVER POWER IC

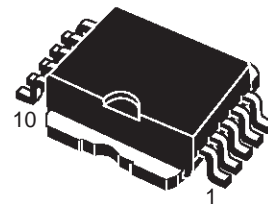
TYPE	V _{clamp}	I _{cl}	I _{lim}
VB027ASP	345 V	9.5 A	160 mA

- PRIMARY COIL VOLTAGE INTERNALLY SET
- COIL CURRENT LIMIT INTERNALLY SET
- LOGIC LEVEL COMPATIBLE INPUT
- DRIVING CURRENT QUASI PROPORTIONAL TO COLLECTOR CURRENT
- DOUBLE FLAG-ON COIL CURRENT

DESCRIPTION

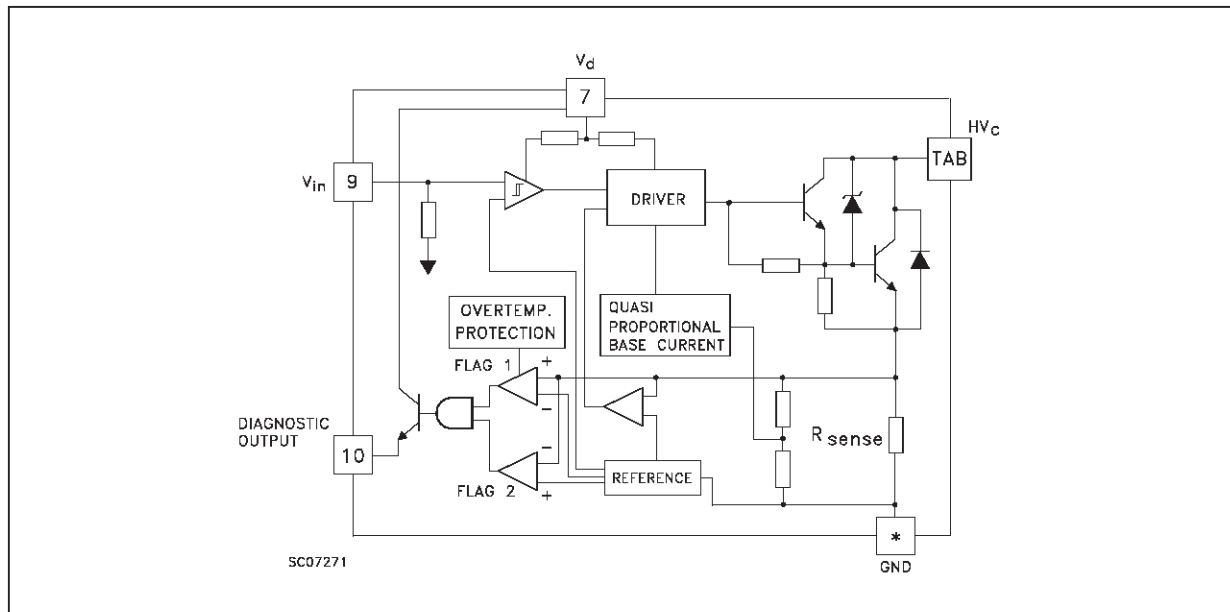
The VB027ASP is a high voltage power integrated circuits made using STMicroelectronics Vertical Intelligent Power Technology, with vertical current flow power darlington and logic level compatible driving circuits.

Built-in protection circuits for coil current limiting and collector voltage clamping allows the VB027ASP to be used as a smart, high voltage, high current interface in advanced electronic ignition systems.



Power SO-10™

BLOCK DIAGRAM



* Pins 1-5 = Power GND, Pin 6 signal GND. Pin 6 must be connected to pins 1-5 externally.

VB027ASP

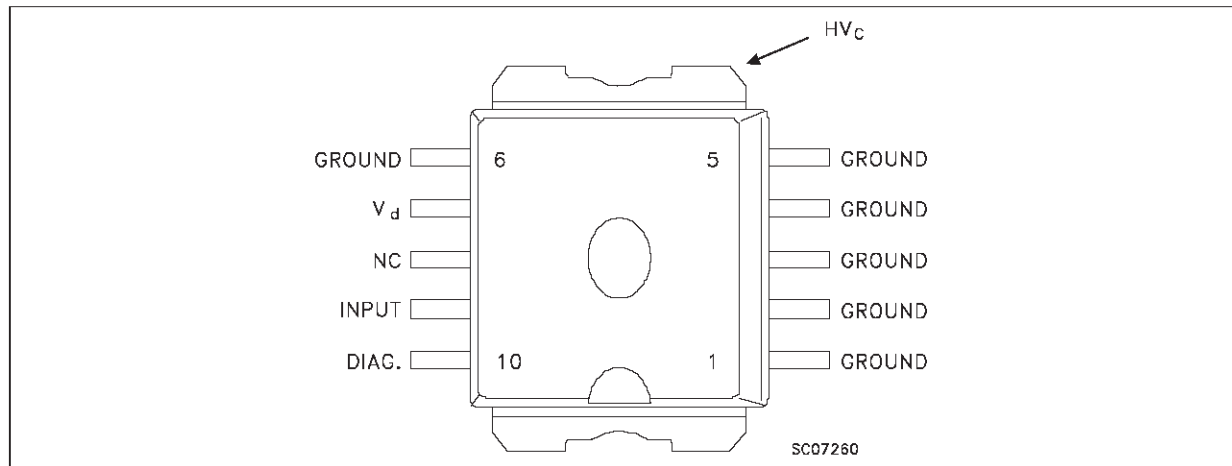
ABSOLUTE MAXIMUM RATING

Symbol	Parameter	Value	Unit
HV_C	Collector Voltage	Internally Limited	V
I_C	Collector Current	Internally Limited	A
V_d	Driving Stage Supply Voltage	7	V
I_d	Driving Circuitry Supply Current	200	mA
V_{in}	Maximum Input Voltage	10	V
T_j	Operating Junction Temperature	-40 to 150	°C
T_{stg}	Storage Temperature Range	-55 to 150	°C

THERMAL DATA

$R_{thj-case}$	Thermal Resistance Junction Case(MAX)	1.12	°C/W
$R_{thj-amb}$	Thermal Resistance Junction Ambient(MAX)	62.5	°C/W

CONNECTION DIAGRAM



PIN FUNCTION

No	NAME	FUNCTION
1 - 5	GND	Emitter Power Ground
6 (*)	GND	Control Ground
7	V_d	Supply Voltage For The Power Stage
TAB	HV_C	Output to The Primary Coil
9	INPUT	
10	DIAGNOSTIC	Output of a Logic Signal When I_C Is Greater Than 3 A

(*) PIN 6 must be connected to PINS 1 - 5 externally

ELECTRICAL CHARACTERISTICS ($V_b = 13.5\text{ V}$; $V_d = 5\text{ V}$; $T_j = 25\text{ }^\circ\text{C}$; $R_{\text{coil}} = 510\text{ m}\Omega$;
 $L_{\text{coil}} = 7\text{ mH}$; unless otherwise specified)

Symbol	Parameter	Test Conditions	Min.	Typ.	Max.	Unit
V_{cl}	High Voltage Clamp	$-40\text{ }^\circ\text{C} \leq T_j \leq 125\text{ }^\circ\text{C}$ $I_{\text{coil}} = 7\text{ A}$	300		400	V
V_{cl}	High Voltage Clamp	$I_{\text{coil}} = 7\text{ A}$	325	345	365	V
$V_{\text{ce(sat)}}$	Saturation Voltage of The Power Stage	$I_c = 7\text{ A}$; $V_{\text{in}} = 4\text{ V}$ $-40\text{ }^\circ\text{C} \leq T_j \leq 125\text{ }^\circ\text{C}$			3	V
$V_{\text{ce(sat)}}$	Saturation Voltage of The Power Stage	$I_c = 6\text{ A}$; $V_{\text{in}} = 4\text{ V}$ $-40\text{ }^\circ\text{C} \leq T_j \leq 125\text{ }^\circ\text{C}$			2	V
$I_{\text{d(stdby)}}$	Stand-by Supply Current	$V_{\text{in}} = 0.4$			11	mA
$I_{\text{d(ugnd)}}$	Stand-by Supply Current During Underground	$V_{\text{in}} = 0.4\text{ V}$ $I_c = -4.5\text{ A}$ $-40\text{ }^\circ\text{C} \leq T_j \leq 125\text{ }^\circ\text{C}$			160	mA
$I_{\text{d(on)}}$	Power On Supply Current	$V_{\text{in}} = 4\text{ V}$ $I_c = 6\text{ A}$ $-40\text{ }^\circ\text{C} \leq T_j \leq 125\text{ }^\circ\text{C}$			130	mA
$I_{\text{d(on)}}$	Power On Supply Current	$V_{\text{in}} = 4\text{ V}$ $I_c = 7\text{ A}$ $-40\text{ }^\circ\text{C} \leq T_j \leq 125\text{ }^\circ\text{C}$			160	mA
V_d	Driver Stage Supply Voltage		4.5		5.5	V
I_{cl}	Coil Current Limit	$V_{\text{in}} = 4\text{ V}$	8.5		10	A
$I_{\text{cl(td)}}$	Coil Current Limit Drift With Temperature	See figure 3				
I_{leak}	Collector Leakage Current	$V_c = 125\text{ V}$			100	μA
V_{inH}	High Level Input Voltage		4		5.5	V
V_{inL}	Low Level Input Voltage		0		0.8	V
I_{inH}	High Level Input Current				200	μA
V_{diagH}	High Level Diagnostic Output Voltage	$R_{\text{EXT}} = 15\text{ K}\Omega$ $C_{\text{EXT}} = 1\text{ nF}$ (see fig. 1)	3.5		V_d	V
V_{diagL}	Low Level Diagnostic Output Voltage	$R_{\text{EXT}} = 15\text{ K}\Omega$ $C_{\text{EXT}} = 1\text{ nF}$ (see fig. 1)			0.5	V
I_{diagTH1}	Diagnostic Current First Threshold		4.25	4.5	4.75	A
I_{diagTD1}	Diagnostic Current First Threshold Drift With Temperature	See figure 4				
I_{diagTH2}	Diagnostic Current Second Threshold		5.45	5.8	6.15	A
I_{diagTD2}	Diagnostic Current Second Threshold Drift With Temperature	See figure 5				
I_{diagH}	Overtemperature Diagnostic Current		2	2.6	3.2	A
t_{dlc}	Delay Time Coil Current	$I_c = 7\text{ A}$	5	25	45	μs
t_{flc}	Fall Time Coil Current	$I_c = 7\text{ A}$	2	8	15	μs
$E_{\text{s/b}}$	Inductive Energy	$V_{\text{CL}} = 400\text{ V}$ $I_c = 7\text{ A}$ $L = 8\text{ mH}$	300			mJ
T_{int}	Temperature of Diagnostic Shift		130	150	170	$^\circ\text{C}$
T_{hys}	Thermal Hysteresis			30		$^\circ\text{C}$
V_F	Forward Voltage of The Body Diode	$I_c = -10\text{ A}$	1.2	2.2	3.2	V

PRINCIPLE OF OPERATION

The VB027ASP is mainly intended as a high voltage power switch device driven by a logic level input and interfaces directly to a high energy electronic ignition coil.

The input V_{in} of the VB027ASP is fed from a low power signal generated by an external controller that determines both dwell time and ignition point.

During V_{in} high ($\geq 4V$) the VB027ASP increases current in the coil to the desired, internally set current level.

After reaching this level, the coil current remains constant until the ignition point, that corresponds to the transition of V_{in} from high to low (typ. 1.9V threshold).

During the coil current switch-off, the primary voltage HV_c is clamped at an internally set value V_{cl} , typically 345V.

The transition from saturation to desaturation, coil current limiting phase, must have the ability to accommodate an overvoltage. A maximum overshoot of 20V is allowed.

THERMAL BEHAVIOUR

You can see in the block diagram of the VB027ASP a box called overtemperature protection. The purpose of this circuit is to shift the current level at which the 1st diagnostic is activated down of about 2.5A.

This information can be managed by the micro that can take the corrective actions in order to reduce the power dissipation.

This block is not an effective protection but just

an overtemperature detection. The shift down of the 1st flag level cannot be present for temperatures lower than 125°C.

As an example of its behaviour you can suppose a very simple motor management system in which the micro does just a simple arithmetic calculation to decide when to switch off the device after the 1st flag threshold.

EXAMPLE:

Iflag info after X msec. (Iflag = 4.5A)

Iswitch off after $K \cdot X$ msec.

As soon as the temperature rises over the overtemp. threshold, the 1st diagnostic is shifted down to about 2.5A and in this example, the switch off current will be $K \cdot X \cdot 2.5 / 4.5$ helping the system to reduce the power dissipation.

As you can see this behaviour is not a protection but just a feedback for the micro.

FEEDBACK

When the collector current exceeds 4.5A, the feedback signal is turned high and it remains so, until the load current reaches 5.8A (second threshold), at that value, the feedback signal is turned low.

OVERVOLTAGE

The VB027BSP can withstand the following transients of the battery line:

-100V/2msec ($R_i = 10 \Omega$)

+100V/0.2msec ($R_i = 10 \Omega$)

+50V/400msec ($R_i = 4.2 \Omega$, with $V_{IN} = 3V$)

FIGURE 1: Application Circuit

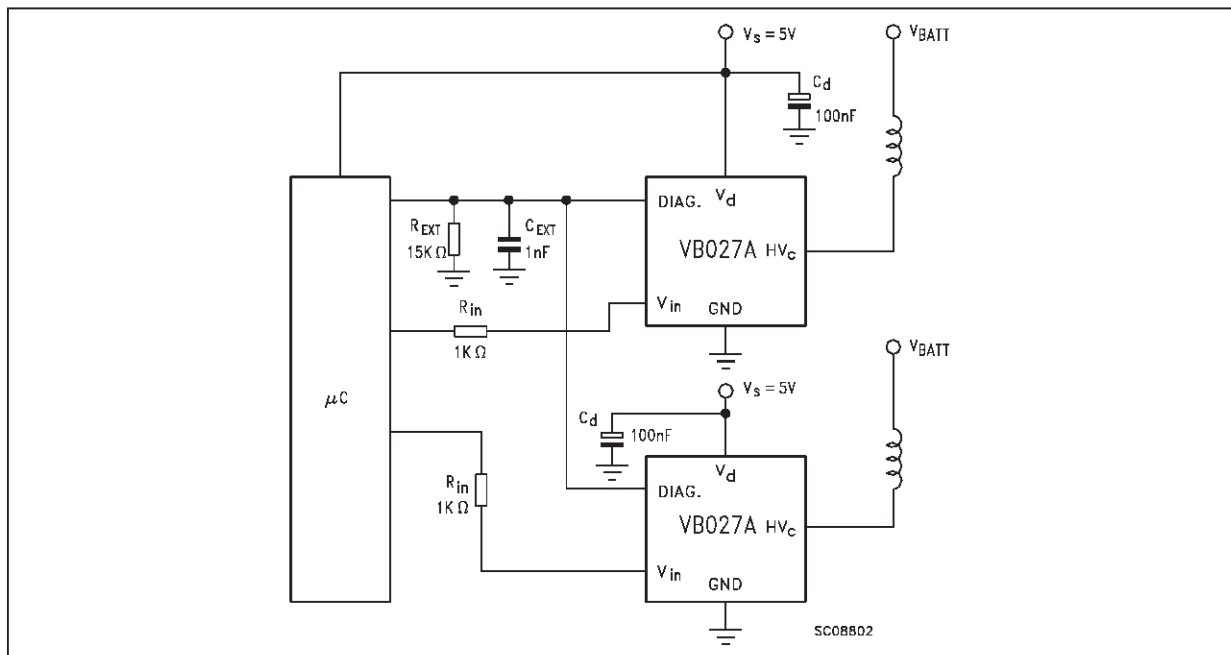


FIGURE 2: Switching Waveforms

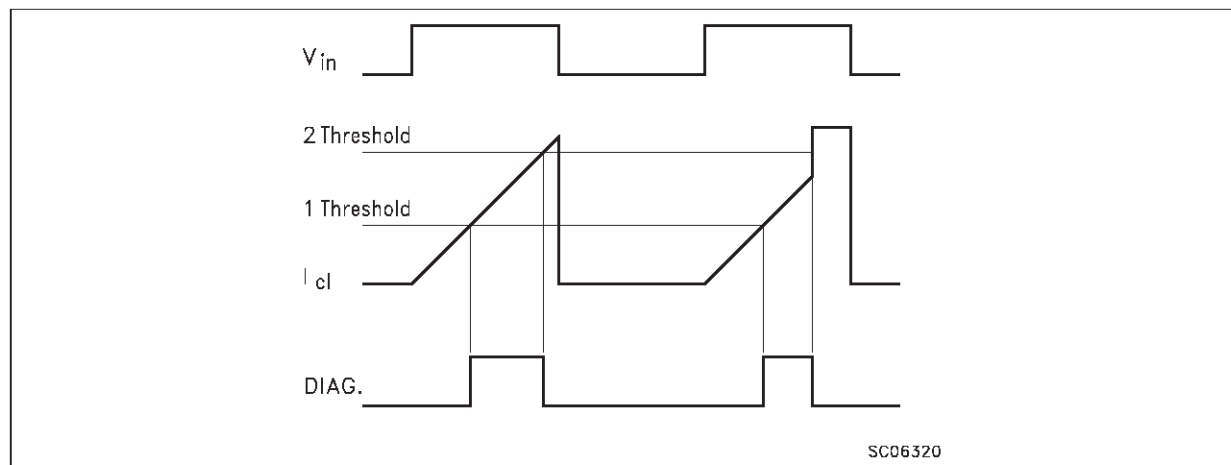


FIGURE 3: Maximum I_{cl} Versus Temperature

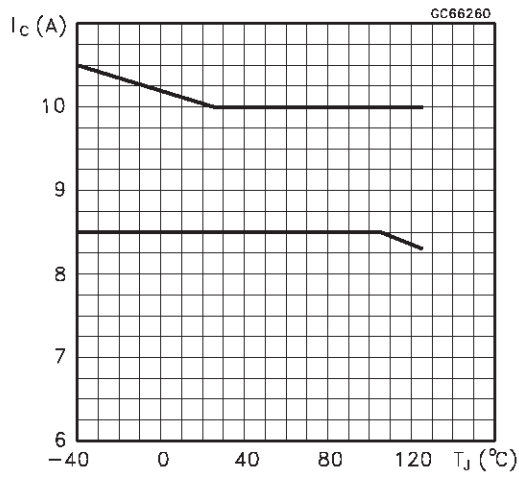


FIGURE 4: I_{flag1} Versus Temperature

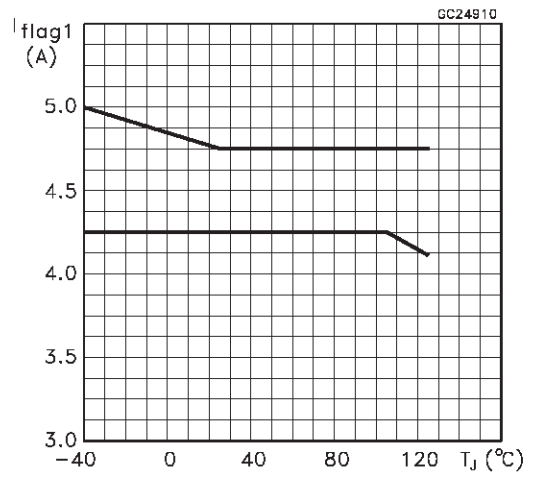
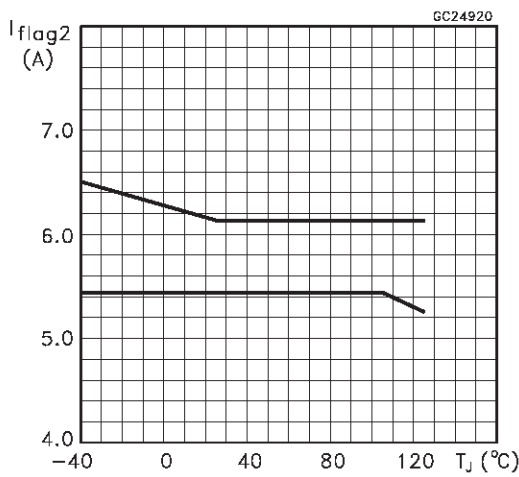
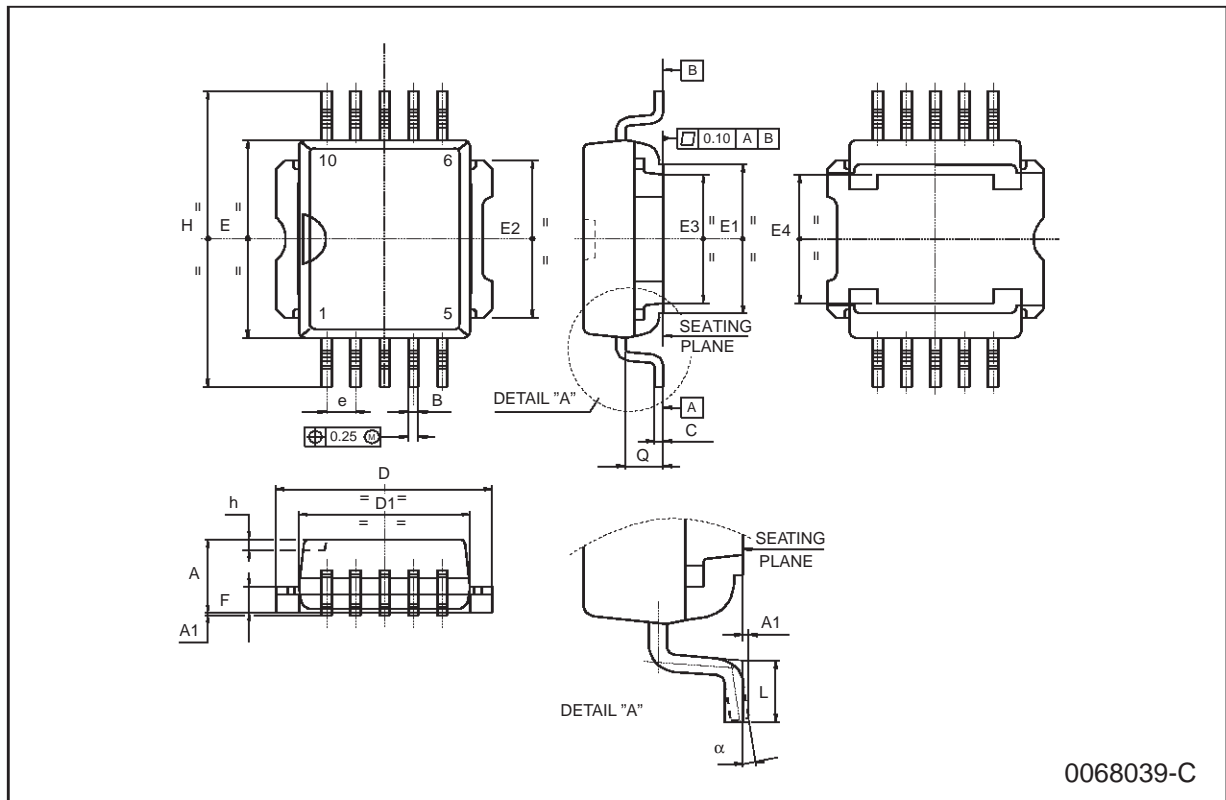


FIGURE 5: I_{flag2} Versus Temperature



PowerSO-10 MECHANICAL DATA

DIM.	mm			inch		
	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.
A	3.35		3.65	0.132		0.144
A1	0.00		0.10	0.000		0.004
B	0.40		0.60	0.016		0.024
C	0.35		0.55	0.013		0.022
D	9.40		9.60	0.370		0.378
D1	7.40		7.60	0.291		0.300
e		1.27			0.050	
E	9.30		9.50	0.366		0.374
E1	7.20		7.40	0.283		0.291
E2	7.20		7.60	0.283		0.300
E3	6.10		6.35	0.240		0.250
E4	5.90		6.10	0.232		0.240
F	1.25		1.35	0.049		0.053
h		0.50			0.002	
H	13.80		14.40	0.543		0.567
L	1.20		1.80	0.047		0.071
q		1.70			0.067	
α	0°		8°			



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